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# Solubility of Eskisehir thorium/rare earth ores in sulphuric and nitric acids

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**Abstract:** Nuclear energy is considered as one of the most important energy resources in the world. Thorium (Th) has a significant potential to be used in electricity production by nuclear energy since its existence is not depended on the presence of another radioactive elements, and it has larger potential reserves than uranium. Bastnaesite ((Ce, La)CO<sub>3</sub>F) is one of the minerals from which Th can be economically extracted. In this study, solubility of bastnaesite containing ore obtained from Eskisehir, Turkey was investigated by leaching with  $H_2SO_4$  and  $HNO_3$  in terms of leaching performance of thorium and some rare-earth elements (Ce, Nd, La). In this context, representative samples were taken from three different areas in Eskisehir-Kizilcaoren region, and a composite sample was prepared to be used for the leaching experiments. The effects of several parameters such as the solid ratio, leaching time, acid amount and pulp temperature, on dissolution efficiencies of Th, Nd, Ce and La was investigated. The best results were obtained using 3.42 mol/dm<sup>3</sup> HNO<sub>3</sub>, solid-to-liquid ratio of 35%, 120 min leaching time and 60 °C temperature. Under these optimum conditions, the dissolution efficiencies of Th, Ce, Nd, and La were obtained as 94%, 82%, 77% and 70%, respectively.

Keywords: thorium, rare earth elements, bastnaesite, leaching, solubility

## 1. Introduction

Thorium exists in quite a prominent position especially in terms of nuclear energy. Thorium is a potential nuclear fuel because <sup>232</sup>Th can be converted to <sup>233</sup>U by absorbing slow neutrons. It is also considered as the cleanest nuclear power plant fuel as less plutonium and other trans-uranium elements are produced from the thorium fuel cycle compared to the uranium fuel cycle. Therefore, it is intended to be used as a substitute for uranium in nuclear reactors being more environmentally friendly compared to uranium. While thorium-based power plants have not yet been built industrially, thorium-based nuclear power research and development operations are ongoing in various countries as an alternative to uranium. Therefore, the interest in thorium as an energy source has been increased (Ipekoglu, 1983; Kaya and Bozkurt, 2003; Ali et al, 2007; Gui et al., 2014; Kursun et al., 2015; Kursun and Terzi, 2015; USGS, 2016).

Approximately sixty Th-bearing minerals are known in nature and the majority of these minerals have high ratios of rare earth elements (REE). Therefore, thorium is commonly associated with REEs which are very important in production of advanced materials for high technology industries, and mainly obtained as a by-product from distillation of monazite ((Ce, La)PO<sub>4</sub>) and bastnaesite ((Ce, La)CO<sub>3</sub>F). In 2013, exploration and development of rare-earth projects associated with thorium have been continued in Australia, Brazil, Canada, Greenland, India, South Africa, United States and Vietnam. The REEs are a unique group of elements, summarized as lanthanides plus scandium (Sc) and yttrium (Y), regarded as being among the most critical elements that are highly valued for their specialized applications in many modern technologies. Neodymium and dysprosium are used as magnets in wind turbines as well as electric vehicles and lanthanum, cerium, europium, terbium and yttrium for phosphors in energy efficient lights (Eyal and Olander, 1990a; Eyal and Olander, 1990b;

Eyal and Olander, 1990c; Ishikawa et al., 2002; Ali et al, 2007; Hingant et al., 2009; Gaiotte et al., 2011; Gok and Aytas, 2013; Lu et al., 2016; USGS, 2016).

There are several hydrometallurgical methods for extracting thorium and REEs from bastnaesite, which is the most industrially important rare earth mineral with the content of rare earth oxides (REOs) and Th equal to 67-73% and 0.2-0.3%, respectively. Presently, bastnaesite concentrates are obtained from gravity and flotation processes commonly treated by calcination-acid dissolution or directly by acid dissolution or alkaline roasting, including H<sub>2</sub>SO<sub>4</sub> acid-roasting and water leaching, HCl acid leaching, HNO<sub>3</sub> acid leaching, Na<sub>2</sub>CO<sub>3</sub> roasting and chlorination. The rare-earth extraction process uses either one or more reagents to decompose the minerals, and to leach the REEs into the solution. The commonly used acids include sulfuric acid (H<sub>2</sub>SO<sub>4</sub>), hydrochloric acid (HCl) and nitric acid (HNO<sub>3</sub>). Bastnaesite can be decomposed into REOs and rare earth fluoride oxide at 400-560 °C, which can be dissolved by sulphuric, nitric and hydrochloric acids at room temperature. On the other hand, Th is soluble in HCl and H<sub>2</sub>SO<sub>4</sub> but insoluble in water. Thorium compounds with fluoride, iodide, phosphate etc. ions are also slightly soluble in acids (Ipekoglu, 1983; Zhang and Saito, 1998; Ozbayoglu and Atalay, 2000; Kaya and Bozkurt, 2003; Yorukoglu et al., 2003; Zhang et al., 2004; Castor and Hedrick, 2006; Bian et al., 2011; Wang et al., 2013; Gui et al., 2014; Huang et al., 2014; ATSDR, 2016; Huang et al., 2016; Machacek and Kalvig, 2016; Ogata et al., 2016; Stone et al., 2016; USGS, 2016; Zhang et al., 2016).

In this study, solubility of bastnaesite containing ore obtained from Eskisehir, Turkey by leaching with  $H_2SO_4$  and  $HNO_3$  was investigated in terms of leaching performance of thorium and some REEs (Ce, Nd, and La).

#### 2. Materials and methods

### 2.1 Materials

The samples subjected to the experimental studies were representatively taken from three different areas in Eskisehir-Kizilcaoren region. The results of preliminary characterization studies showed that the samples had similar features in terms of their mineralogical and chemical compositions. Therefore, some composite samples were prepared by mixing equal weight ratios of the samples to be used in the experiments. Subsequently, the characterization experiments were performed in order to determine the physical, chemical and mineralogical properties of the sample.

The results of chemical analysis obtained by inductively coupled plasma mass spectrometry (ICP-MS) indicated that La, Ce, Nd, Y, Th, and U contents of the sample were found to be 2.79%, 2.27%, 0.29%, 450 ppm, 0.69%, and 200.3 ppm, respectively. It was determined that the samples contained 0.14% of total moisture, and it can be removed after 90 min of drying in the oven at 105 °C. The samples were subjected to a size analysis after they were crushed in two stages by jaw and roll crushers in order to provide a suitable feed size for leaching. As a result of the sieve analysis,  $d_{50}$  and  $d_{80}$  of the sample were determined as 0.45 mm and 1.58 mm, respectively. Figure 1 shows the Th and REOs contents of the sample as a function of particle size.



Fig. 1. Th and REOs content of sample according to sieve fractions

As seen in Fig. 1, Th and REE oxide contents in the sample were tended to increase inversely proportional to the particle size. The highest distribution was obtained in the -38  $\mu$ m size fraction, and the assay values of La<sub>2</sub>O<sub>3</sub>, CeO<sub>2</sub>, Nd<sub>2</sub>O<sub>3</sub>, and ThO<sub>2</sub> in this fraction were found as 23.11%, 7.17%, 1.90%, and 4.09%, respectively. The obtained results suggested that the liberation degree of bastnaesite, which was the dominant Th and REOs source in the sample, increased in finer particle sizes, thus, Th and REO contents tended to be concentrated in the finer fractions. The specific gravity of the sample was found as 3.29 g/cm<sup>3</sup>.

The pH change of the sample in the purified water depending on the time was analyzed in order to identify the electrokinetic properties of the sample. The pH profiles of the sample are shown in Fig. 2.



Fig. 2. pH profile of the sample

As seen from Fig. 2, the pH value of the sample at pH 3, 8, 10 and 11 started reaching a buffer pH value in the alkaline regions after a certain time. No change depending on the time was observed at pH 2 which was the highest acidic pH value analyzed in the experiments. The reason of this can be explained by the limited amount of the anions formed by dissolving from the sample in a high acidic medium.

In order to determine the mineralogical composition of the sample, the X-ray diffraction analysis (XRD) was performed (Fig. 3). The results of XRD analysis showed that the sample contained high rates of fluorite-CaF<sub>2</sub> and plumbian-barite (Ba, Pb)SO<sub>4</sub>. Bastnaesite and some other minerals, which exist within the mineralogical composition in the sample, could not be seen by XRD due to the detection limits of the method.



Fig. 3. XRD diffraction pattern of the sample

#### 2.2 Methods

The leaching experiments were carried out in Erlenmeyer flasks using a shaking water bath (Witeg, Germany), and the shaking speed, pH, and pulp temperature were controlled periodically during the experiments. The values of pH and pulp temperature were controlled periodically during the experiments. In the leaching processes,  $H_2SO_4$  at 96-98% purity (Tekkim, Turkey) and HNO<sub>3</sub> at 55-57% purity (Tekkim, Turkey) were used. The particle size of the feed samples was 106 µm, which were obtained from the closed circuit grinding in a steel ball mill. After the leaching process, solid-liquid separation was carried out using filter papers with pores size of 4 µm. The obtained filter cake was washed in 2 steps with 1% (w/w) acid solution, then Th and REE contents were analyzed by the ICP-MS method. The dissolution efficiency (D.E.) was calculated according to formula:

$$D.E.\% = \frac{Th,REE in the feed - Th,REE in the f.cake}{Th,REE in the feed} \cdot 100.$$
(1)

The effects of several parameters such as the solid-to-liquid ratio, leaching time, acid amount and pulp temperature on dissolution efficiencies of Th, Nd, Ce, and La were investigated under different conditions of 15-50% solid ratio, 30-320 min leaching time, 0.137-4.38 (H<sub>2</sub>SO<sub>4</sub>), 0.214-6.85 (HNO<sub>3</sub>) mol/dm<sup>3</sup> concentration, and 25-90°C leaching temperature.

## 3. Results and discussion

#### 3.1 Effect of solid-to-liquid ratio

The dissolution efficiency of Th, Ce, Nd, and La as a function of solid-to-liquid ratio for  $H_2SO_4$  and  $HNO_3$  leaching are shown in Fig. 4. The dissolution efficiencies of all investigated elements increased up to 35% solid ratio in a similar manner with both  $H_2SO_4$  and  $HNO_3$ . After this point, the solubility of Th, Ce and La significantly decreased especially for  $H_2SO_4$  leaching. On the other hand, the dissolution efficiencies followed a relatively stable trend after this point for  $HNO_3$  leaching. This was probably due to the relative decrease in the amount of solvent per unit of solids due to the increase in the solid ratio and the lack of sufficient solvent amount to dissolve the target contents in the aqueous media in the high solids ratio.

It was also observed that the diffusion and mixing problems began to arise as the viscosity of the pulp increased. The obtained results showed that the solid ratio had no positive effect on the dissolution efficiency after a certain level. According to the results, 35% of solid ratio was found to be optimum for the dissolution efficiency of Th, Ce, Nd, and La.



Fig. 4. Dissolution efficiency of Th, Ce, Nd, and La as a function of solid ratio in (a) H<sub>2</sub>SO<sub>4</sub> (25 °C pulp temperature, 2.19 mol/dm<sup>3</sup> acid dosage, 240 min leaching time) and (b) HNO<sub>3</sub> (25 °C pulp temperature, 2.57 mol/dm<sup>3</sup> acid dosage, 240 min leaching time)

## 3.2 Effect of leaching time

The dissolution efficiency of Th, Ce, Nd, and La as a function of leaching time in  $H_2SO_4$  and  $HNO_3$  is given in Fig. 5. According to the results, it was observed that the leaching time showed a considerable effect on the dissolution efficiency for all elements for both  $H_2SO_4$  and  $HNO_3$  leaching. In  $H_2SO_4$  the dissolution efficiency of 20% at 30 min increased to about 47% for Th and 35% for Ce after 150 min.

A non-linear increase in the dissolution efficiencies was obtained up to 220 min of leaching time, and then no significant increase was observed in  $H_2SO_4$  leaching. On the other hand, the dissolution efficiencies showed an almost linear increase up to 120 min of leaching time, and then they reached a plateau after this point in HNO<sub>3</sub> leaching. The lack of further increase after the certain point was due to completion of dissolution reactions in terms of  $H_2SO_4$  and HNO<sub>3</sub> soluble Th and REE contents. The optimum leaching time in  $H_2SO_4$  and HNO<sub>3</sub> was 220 min and 120 min, respectively.



Fig. 5. Dissolution efficiency of Th, Ce, Nd, and La as a function of leaching time in (a) H<sub>2</sub>SO<sub>4</sub> (35% solid ratio, 25 °C pulp temperature, 2.19 mol/dm<sup>3</sup> acid dosage) and (b) HNO<sub>3</sub> (35% solid ratio, 25 °C pulp temperature, 2.57 mol/dm<sup>3</sup> acid dosage)

## 3.3 Effect of acid dosage

The dissolution efficiency of Th, Ce, Nd, and La as a function of acid amount in  $H_2SO_4$  and  $HNO_3$  is given in Fig. 6. When the effect of acid dosage in  $H_2SO_4$  was examined, it was observed that the dissolution efficiency of Th was more affected by the acid dosage compared to  $HNO_3$  leaching. The dissolution efficiencies of Th and REEs increased up to the acid dosage of 2.19 mol/dm<sup>3</sup>, and after this point, no significant change was observed. On the other hand, a rapid increase in the REE dissolution efficiencies up to acid dosage of 1.71 mol/dm<sup>3</sup> was observed in  $HNO_3$ . Subsequently, even the slope of the dissolution curves reduced, the increase continued up to a plateau point at 3.42 mol/dm<sup>3</sup>. According to these results, it can be concluded that the investigated range of acid amounts was sufficient to dissolve Th and REE, and any further increase in the acid amount would not have significant positive effect. Therefore, the optimum amount of  $H_2SO_4$  and  $HNO_3$  were found to be 2.19 mol/dm<sup>3</sup> and 3.42 mol/dm<sup>3</sup>, respectively.

## 3.4 Effect of pulp temperature

The dissolution efficiency of Th, Ce, Nd, and La as a function of pulp temperature in  $H_2SO_4$  and  $HNO_3$  is shown in Fig. 7. As clearly seen from Fig. 7, the temperature showed no significant effect on the dissolution efficiencies of REEs for leaching with both acids. However, considering its positive effect on the dissolution efficiency of Th, the optimum pulp temperature was determined as 70 °C in  $H_2SO_4$ , at which Th, Ce, Nd and La dissolved with rates of 66.67, 51.04, 43.22 and 40.29%, respectively. Similarly, the increase at the rate of 8% was observed in the dissolution efficiency of Th in  $H_2SO_4$ . Furthermore, the optimum pulp temperature was determined as 60 °C due to the legible differences between the dissolution efficiencies obtained at 60 and 70 °C in HNO<sub>3</sub> leaching experiments.



Fig. 6. Dissolution efficiency of Th, Ce, Nd and La as a function of acid dosage in (a) H<sub>2</sub>SO<sub>4</sub> (35% solid ratio, 25 °C pulp temperature, 220 min leaching time) and (b) HNO<sub>3</sub> (35% solid ratio, 25°C pulp temperature, 120 min leaching time)



Fig. 7. Dissolution efficiency of Th, Ce, Nd, and La as a function of pulp temperature in (a) H<sub>2</sub>SO<sub>4</sub> (35% solid ratio, 2.19 mol/dm<sup>3</sup> acid dosage, 220 min leaching time) and (b) HNO<sub>3</sub> (35% solid ratio, 3.42 mol/dm<sup>3</sup> acid dosage, 120 min leaching time)

## 4. Discussion and conclusions

In this study, the solubility of a bastnaesite containing ore by leaching with H<sub>2</sub>SO<sub>4</sub> and HNO<sub>3</sub> were compared in terms of dissolution efficiencies of Th, Ce, Nd, and La. According to the results, the highest Th dissolution efficiency was obtained as 90.88% and 66.67% in HNO<sub>3</sub> and H<sub>2</sub>SO<sub>4</sub>, respectively. The highest dissolution efficiencies for Ce, Nd, and La were obtained as 51.04%, 43.22%, and 40.29% for H<sub>2</sub>SO<sub>4</sub> leaching, and 77.45%, 67.15%, and 60.22% for HNO<sub>3</sub> acid leaching, respectively. The dissolution efficiencies of the elements by using both acids were obtained from the highest to the lowest as Th, Ce, Nd, and La, respectively. The difference between dissolution efficiencies of Th, Ce, Nd and La can be attributed to the fact that part of these elements might be contained in different species of bastneasite group and other trace REE minerals in the sample, which all differs in their acid solubility properties, as well as to the fact that REE fluorides have different solubility constants as it was presented by Migdisov et al. (2009).

The results obtained in this study are consistent with the results of studies on the dissolution REEs from bastnaesite containing ores for  $H_2SO_4$  and  $HNO_3$  leaching in literature. Feng et al. (2013) performed series of experiments with  $H_2SO_4$ , the highest REE dissolution efficiencies were obtained under the conditions of 1.5 mol/dm<sup>3</sup>. Additionally, most significant effect of temperature increase on the REE dissolution efficiencies were obtained between 30 and 40 °C, while the increase between 60

and 70 °C was negligible similar to this study. Studies conducted by Baroch (1958) on the enrichment of California bastnaesite for HNO<sub>3</sub> leaching showed that the maximum dissolution efficiencies of REEs reached after 2 h of leaching. It was also observed that the increase in the leaching time after this point showed no significant effect on the REEs dissolution efficiencies of REEs. However, the dissolution efficiencies obtained with  $H_2SO_4$  were found to be higher than HNO<sub>3</sub> in several studies on the dissolution of different ores for  $H_2SO_4$  and HNO<sub>3</sub> leaching (Meor, 2013). This can be attributed to the fact that the dissolution efficiency depends on the type of REE-containing phases (ReF<sub>3</sub>/ReCO<sub>3</sub>) as well as gangue minerals present (SiO<sub>2</sub>, CaCO<sub>3</sub>, etc.) in the ore that often affect the leaching process.

It can be concluded that the best result was obtained with HNO<sub>3</sub> leaching under 35% solid ratio,  $3.42 \text{ mol/dm}^3 \text{ HNO}_3$ , 120 min leaching time, and 60 °C pulp temperature when the dissolution rates of Th and REEs taken into consideration together. HNO<sub>3</sub> was more efficient than H<sub>2</sub>SO<sub>4</sub> in terms of Th dissolution as the dissolution efficiency of Th reached 90% at the end of 2 h leaching time with use of  $3.42 \text{ mol/dm}^3 \text{ HNO}_3$ . Under these conditions, the dissolution efficiencies of Th, Ce, Nd, and La were obtained as 90.88%, 77.45%, 67.15%, and 60.22%, respectively. The relatively low leaching efficiencies of REEs can be attributed to poor dissolution capacity of bastnaesite, which has a hexagonal form in acid solutions. It was also observed that the dissolution efficiencies were improved by increasing of dissolution time, while this level of dissolution rates could not be attained with H<sub>2</sub>SO<sub>4</sub> altogether.

In addition to the higher obtained dissolution efficiencies, there are several advantages of HNO<sub>3</sub> over H<sub>2</sub>SO<sub>4</sub> for leaching of Eskisehir thorium/rare earth ores were observed. As a strong acid with a high diffusion constant, HNO<sub>3</sub> does not provide compounds precipitating with cations, thus it dissolves thorium more efficiently than H<sub>2</sub>SO<sub>4</sub>, and the acid consumption for the same efficiency was lower than H<sub>2</sub>SO<sub>4</sub>. Additionally, the use of HNO<sub>3</sub> was positively influenced the dissolution efficiency of Th as it provided no difficulty in mixing and filtration. The result of this study clearly indicated that the leaching method using common mineral acids such as H<sub>2</sub>SO<sub>4</sub> and HNO<sub>3</sub> was a simple and applicable process which provided relatively high dissolution rates in terms of extracting some REEs and especially Th from bastnaesite containing ores.

#### References

- ALI A.M.I., EL-NADI Y.A., DAOUD J.A., ALY H.F.H., 2007. Recovery of thorium (IV) from leached monazite solutions using counter-current extraction. Int. J. Miner. Process., 81, 217-223.
- ATSDR, 2016. Agency for Toxic Substances & Disease Registry. Chem. Phys. Inform., http://www.atsdr.cdc.gov/toxprofiles/tp147-c3.pdf (Last Accessed: 17.04.2017).
- BAROCH C.J., 1958. Processing of California bastnaesite ore. Iowa State Collage, PhD. Dissertation, Iowa, USA.
- BIAN X., YIN S., LUO Y., WU W., 2011. Leaching kinetics of bastnaesite concentrate in HCl solution. Trans. Nonferrous Met. Soc. China, 21, 2306-2310.
- CASTOR S.B., HEDRICK J.B., 2006. *Rare Earth Elements*. Industrial Minerals volume, 7<sup>th</sup> edition, Society for Mining, Metallurgy and Exploration, Littleton, Colorado, 769-792.
- EYAL Y., OLANDER D.R., 1990. Leaching of uranium and thorium from monazite: I. Initial leaching. Geochim. Cosmochim. Acta, 54(7), 1867-1877.
- EYAL Y., OLANDER D.R., 1990. Leaching of uranium and thorium from monazite: II. Elemental leaching. Geochim. Cosmochim. Acta, 54(7), 1879-1887.
- EYAL Y., OLANDER D.R., 1990. Leaching of uranium and thorium from monazite: III. Leaching of radiogenic daughters. Geochim. Cosmochim. Acta, 54(7), 1889-1896.
- FENG X.L., LONG, Z.Q., CUI D.L., WANG L.S., HUANG X.W., ZHANG G.C., 2013. *Kinetics of rare earth leaching from roasted ore of bastnaesite with sulfuric acid.* Trans. Nonferrous Met. Soc. China, 23, 849-854.
- GAIOTTE J.V.M., VILLEGAS R.A.S., FUKUMA H.T., 2011. Uranium and thorium recovery in thorianite orepreliminary results. in: International Nuclear Atlantic Conference, Brazil.
- GOK C., AYTAS S., 2013. Recovery of thorium by high-capacity biopolymeric sorbent. Separ. Sci. Technol., 48, 2115-2124.
- GUI W., ZHANG H., LIU Q., ZHU X., YANG Y., 2014. Recovery of Th (IV) from acid leaching solutions of bastnaesite at low concentrations. Hydrometall., 147-148, 157-163.

- HINGANT H., CLAVIER N., DACHEUX N., BARRE N., HUBERT S., OBBADE S., TABORDA F., ABRAHAM F., 2009. *Preparation, sintering, and leaching of optimized uranium thorium dioxides*. J. Nucl. Mat., 385, 400-406.
- HUANG Y., ZHANG T., DOU Z, LIU J., TANG F., 2014. Study on leaching rare earths from bastnaesite treated by calcification transition. J. Rare Earth., 32(11), 1043-1047.
- IPEKOGLU B., 1983. *Evaluation of Eskisehir-Beylikahir thorium ore*. ITU (Istanbul Technical University) Graduate School of Science Engineering and Technology, PhD. Dissertation, Istanbul, Turkey.
- ISHIKHAWA S., SUYAMA K., ARIHARA K., ITOH M., 2002. Selective recovery of uranium and thorium ions from dilute aqueous solutions by animal biopolymers. Biol. Trace Elem. Res., 86, 227-236.
- KAYA M., BOZKURT V., 2003. Thorium as a nuclear fuel. in: 18<sup>th</sup> International Mining Congress and Exhibition of Turkey – IMCET, 571-578.
- KURSUN I., TERZI M., 2015. Investigation of solubility of radioactive elements contained in ashes of Yatagan Thermal Power Plant in acetic acid. Asian J. Chem., 27, 2685-2690.
- KURSUN I., TERZI M., ENKHTAIVAN N., TOMBAL T.D., 2015. *Recovery of radioactive elements from a coal fly ash by HCl leaching method*. in: International Energy Raw Materials and Energy Summit, Istanbul, Turkey.
- LU Y., WEI H., ZHANG Z., LI Y., WU G., LIAO W., 2016. Selective extraction and separation of thorium from rare earths by a phosphorodiamidate extractant. Hydrometall., 163, 192-197.
- MACHACEK E., KALVIG P., 2016. Assessing advanced rare earth element-bearing deposits for industrial demand in the *EU*. Resour. Policy, 49, 186-203.
- MEOR, Y., 2013. Rate of rare earths leaching in HCl, H<sub>2</sub>SO<sub>4</sub> and HNO<sub>3</sub>. Adv. Mat. Res., 795, 1-4.
- MIGDISOV, A. A., WILLIAMS-JONES, A. E., WAGNER, T., 2009. An experimental study of the solubility and speciation of the Rare Earth Elements (III) in fluoride-and chloride-bearing aqueous solutions at temperatures up to 300°C. Geochim. Cosmochim. Acta, 73(23), 7087-7109.
- OGATA T., NARITA N., TANAKA M., 2016. Adsorption mechanism of rare earth elements by adsorbents with diglycolamic acid ligands. Hydrometall., 163, 156-160.
- OZBAYOGLU G., ATALAY M.U., 2000. Beneficiation of bastnaesite by a multi-gravity separator. J. Alloys Comp., 303-304, 520-523.
- STONE K., BANDARA A.M. T.S., SENANAYAKE G., JAYASEKERA S., 2016. Processing of rare earth phosphate concentrates: a comparative study of pre-leaching with percloric, hydrochloric, nitric and phosphoric acids and deportment of minor/major elements. Hydrometall., 163, 137-147.
- USGS, 2016, Thorium, http://minerals.usgs.gov/minerals/pubs/commodity/thorium/mcs-2016-thori.pdf (Last Accessed: 17.04.2017).
- WANG L., YU Y., HUANG X., LONG Z., CIU D., 2013. Toward greener comprehensive utilization of bastnaesite: simultaneous recovery of cerium, fluorine, and thorium from bastnaesite leach liquor using HEH(EHP). Chem. Eng. J., 215-216, 162-167.
- YORUKOGLU A., OBUT A., GIRGIN I., 2003. Effect of thiourea on sulphuric acid leaching of bastnaesite. Hydrometall., 68, 195-202.
- ZHANG J., ZHAO B., SCHREINER B., 2016. Separation hydrometallurgy of rare earth elements. Springer International Publishing Switzerland.
- ZHANG L.Q., WANG Z.C., TONG S.X., LEI P.X., ZOU W., 2004. Rare earth extraction from bastnaesite concentrate by stepwise carbochlorinaion-chemical vapor transport-oxidation. Metall. Mat. Trans. B, 35B, 217-221.
- ZHANG Q., SAITO F., 1998. Non-thermal process for extracting rare earths from bastnaesite by means of mechanochemical treatment. Hydrometall., 47, 231-241.